

ECE 3250

Electromagnetic Energy Conversion

Lecture 23: Induction Machine Measurements

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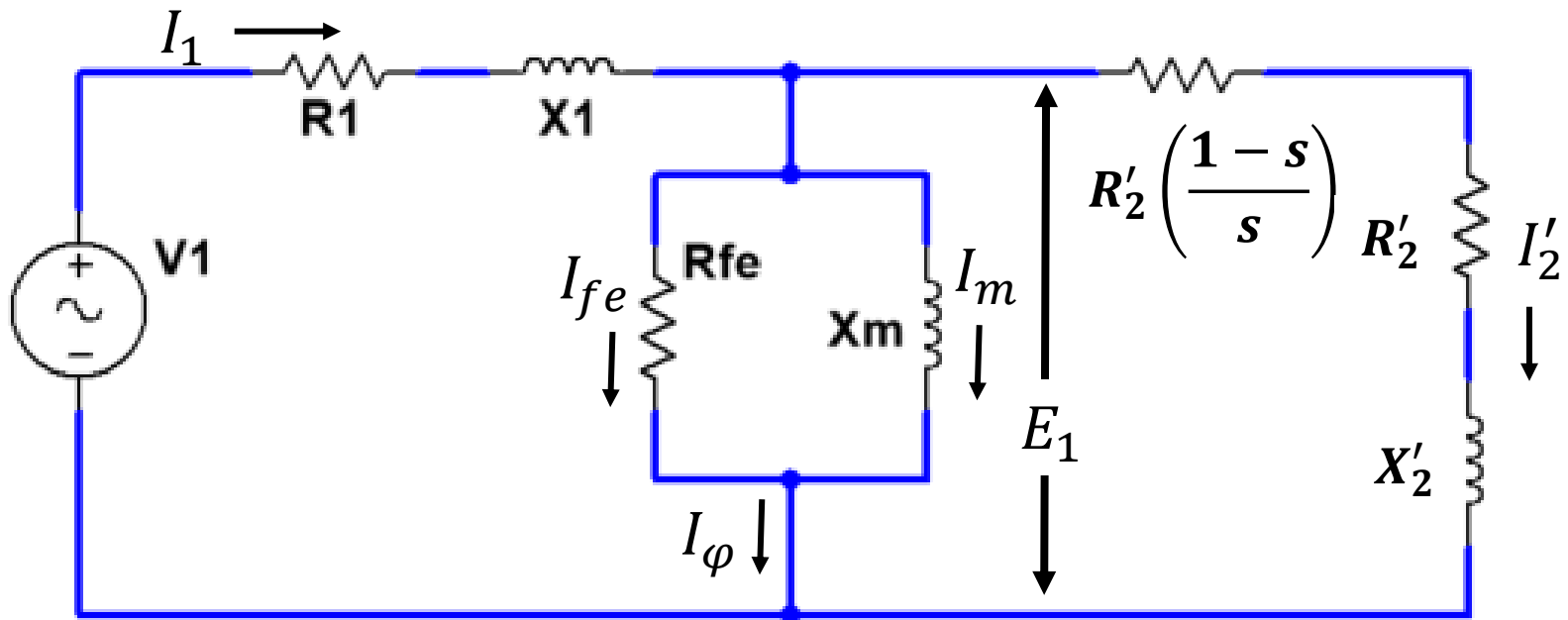
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Today's Agenda

- Induction machines: taking measurements
 - No load test
 - Locked rotor test
- Induction machine efficiency

Induction Machine Circuit Model

- How do we find our induction machine circuit parameters?



Transformer vs. Motor Test

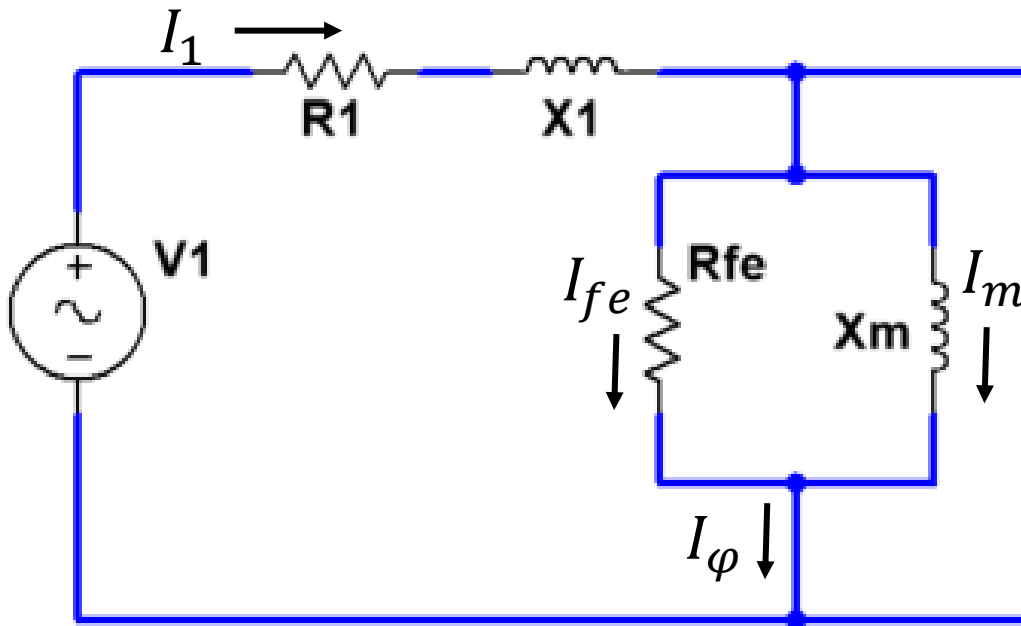
Transformer	Parameters	Motor	Parameters
Open Circuit Test	$R_{fe} \text{ \& } jX_M$	No load test (done at rated voltage)	$R_{fe} \text{ \& } jX_M$ (stator)
Short Circuit Test	$R_{cu} \text{ \& } jX_L$	Locked rotor test (done at rated current)	$R'_2 \text{ \& } jX'_2$ (rotor)

An induction machine with no load has the rotor effectively spinning at the synchronous speed, so slip $s \approx 0$, and our $R'_2 \left(\frac{1-s}{s} \right)$ term looks like an open circuit in our model

The locked-rotor induction motor is basically the same as a three-phase transformer with the stator windings acting as the primary. The rotor conductors act as short-circuited secondary windings.

No Load Test

- With no load the rotor side of the circuit is effectively removed.
- We assume that $R_1 \ll R_{fe}$ and $X_1 \ll X_m$ so losses are due almost entirely to R_{fe} and X_m



No Load Test

- If there is no load on the motor, the torque is nearly zero, and the slip is also nearly zero.

$$\tau \approx 0 \qquad s \approx 0 \qquad \omega_m \approx \omega_s \qquad I_2 \approx 0$$

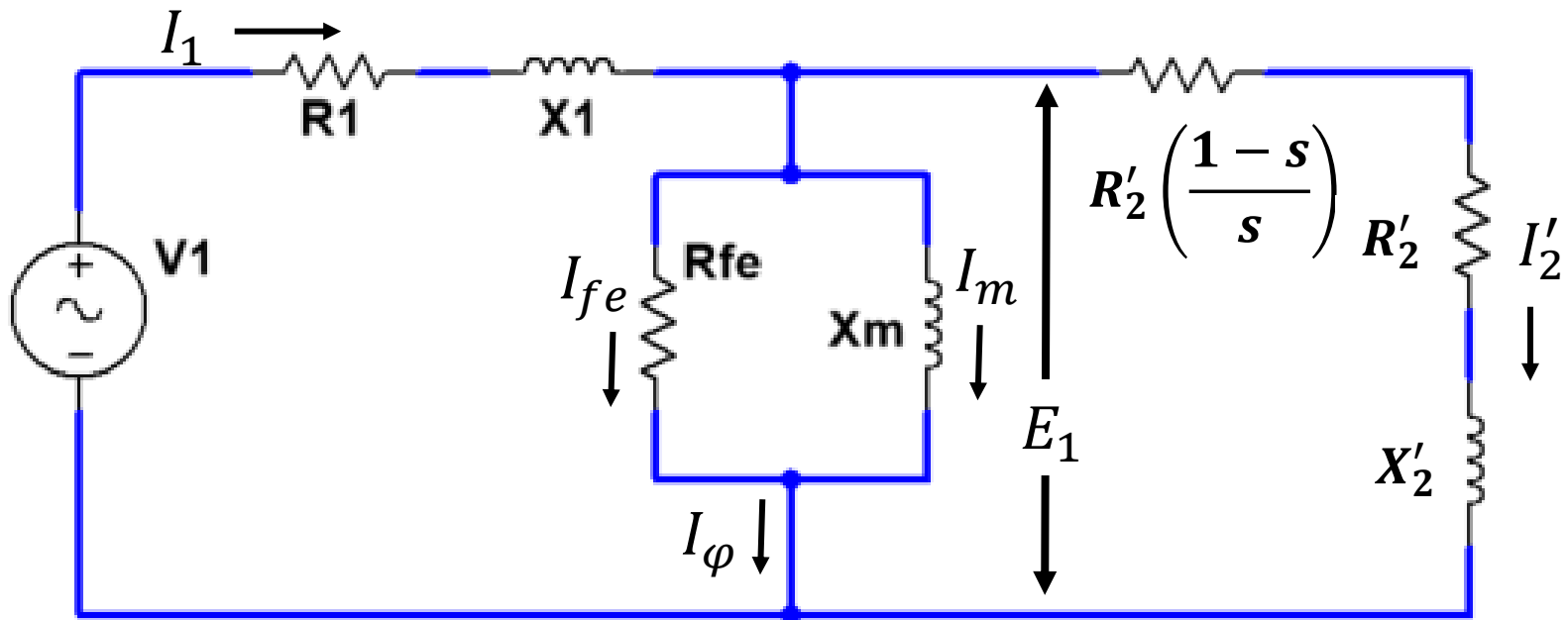
$$R_{fe} = \frac{(V_{NL})^2}{P_{NL}} \qquad Q = \sqrt{(VI)^2 - P^2} \qquad X_m = \frac{(V_{NL})^2}{Q_{NL}}$$

- Be careful to keep line and phase values straight! Since the motor is wye connected:

$$V_{phase} = \frac{V_{line}}{\sqrt{3}}$$

Locked Rotor Test

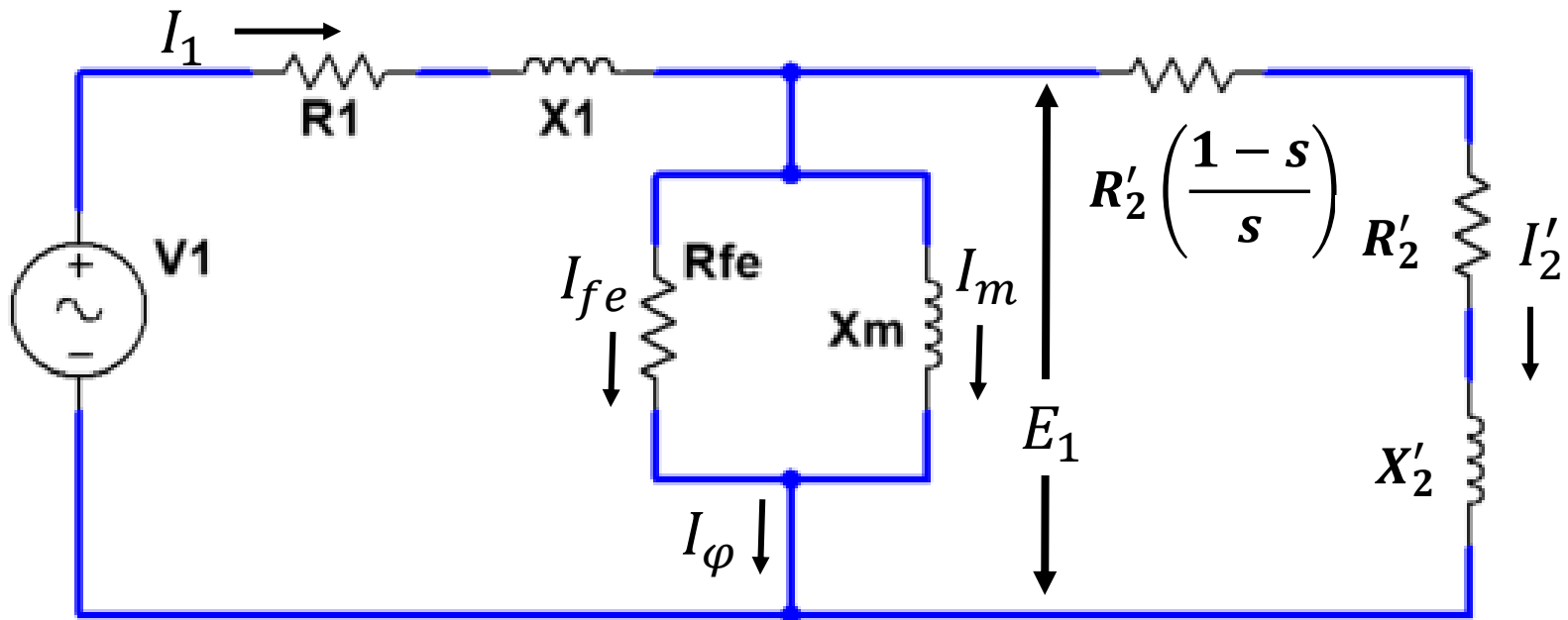
- With the rotor locked, slip = 1, so $R'_2 \left(\frac{1-s}{s} \right) = 0$
- We assume $R'_2 \ll R_{fe}$ and $X'_2 \ll X_m$, so $I_1 \approx I'_2$ and there is almost no current in the core, so the core doesn't contribute to any losses



Locked Rotor Test

$$R_{eq} = R_1 + R'_2 = \frac{P_{LR}}{(I_{LR})^2}$$

$$X_{eq} = X_1 + X'_2$$

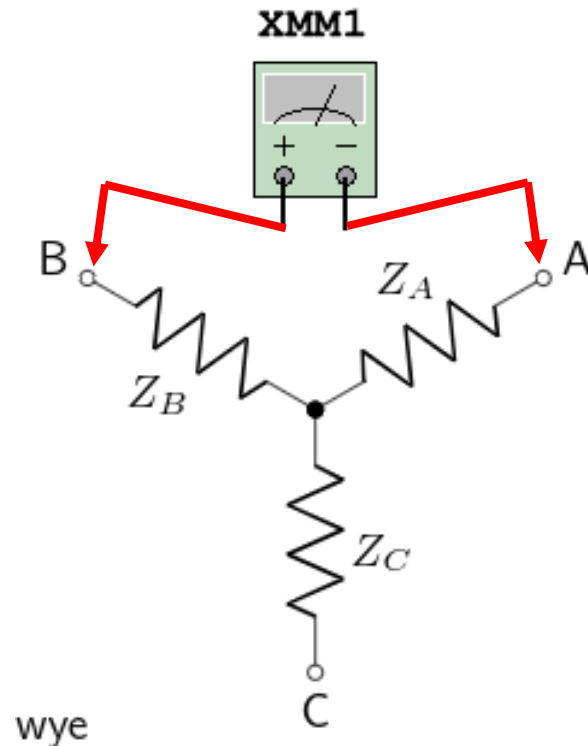


Measuring Motor Parameters

- Nearly all small motors are wye-connected and $Z_A = Z_B = Z_C$
- We can measure the resistance of the stator, R_1 , with an ohm-meter, which measures only the resistance, not the inductance

$$R_1 = \frac{R_A + R_B}{2} = \frac{2R_A}{2} = R_A$$

$$R'_2 = R_{eq} - R_1$$



Locked Rotor Test

- To find the reactance, we go back to Ohm's Law

$$|Z_{eq}| = \frac{V_{LR}}{I_{LR}} \quad X_{eq} = \sqrt{(Z_{eq})^2 - (R_{eq})^2}$$

$$X_{eq} = X_1 + X_2'$$

- Here we follow an approximation that $X_1 = X_2' = \frac{X_{eq}}{2}$

Induction Motor Example

- Given a motor with the following ratings, determine test values and find the motor parameters:
- Rated Voltage: 208 V
- Rated Current: 2.77 A
- Rated Speed: 1710 rpm
- 4 pole
- Wye connected



	No Load Test (Rated Voltage)	Locked Rotor Test (Rated Current)
V	208 V	27 V
I	1.562 A	2.77 A
P	450 W	59.4 W

Induction Motor Example

- From the No Load Test

$$V_1 = \frac{V_{line}}{\sqrt{3}} = \frac{208V}{\sqrt{3}} = 120V$$

$$P_{phase} = \frac{P_{3p}}{3} = \frac{450W}{3} = 150W$$



	No Load Test (Rated Voltage)	Locked Rotor Test (Rated Current)
V	208 V	27 V
I	1.562 A	2.77 A
P	450 W	59.4 W

Induction Motor Example

- From the No Load Test

$$V_1 = 120V \quad P_{phase} = 150W$$



$$R_{fe} = \frac{(V_{NL})^2}{P_{NL}} = \frac{(120V)^2}{150W} = 96\Omega$$

$$Q = \sqrt{(VI)^2 - P^2} = \sqrt{(120V \cdot 1.562A)^2 - (150W)^2} = 112VAR$$

$$jX_m = j \frac{(V_{NL})^2}{Q_{NL}} = j \frac{(120V)^2}{112VAR} = j128\Omega$$

Induction Motor Example

- From the Locked Rotor Test

$$V_1 = \frac{V_{line}}{\sqrt{3}} = \frac{27V}{\sqrt{3}} = 15.58V$$

$$P_{phase} = \frac{P_{3p}}{3} = \frac{59.4W}{3} = 19.8W$$

$$\begin{aligned} R_{eq} &= \frac{P_{LR}}{(I_{LR})^2} \\ &= \frac{19.8W}{(2.77A)^2} \\ &= 2.58\Omega \end{aligned}$$



	No Load Test (Rated Voltage)	Locked Rotor Test (Rated Current)
V	208 V	27 V
I	1.562 A	2.77 A
P	450 W	59.4 W

Induction Motor Example

- From direct measurement of the line-to-line resistance we find:

$$R_{line} = 2.4\Omega \quad R_1 = \frac{R_{line}}{2} = 1.2\Omega$$

$$R'_2 = R_{eq} - R_1$$

$$R'_2 = 2.58\Omega - 1.2\Omega = 1.38\Omega$$



Induction Motor Example

- To find the reactive components we continue using the Locked Rotor Test values

$$|Z_{eq}| = \frac{V_{LR}}{I_{LR}} = \frac{15.58V}{2.77A} = 5.63\Omega$$



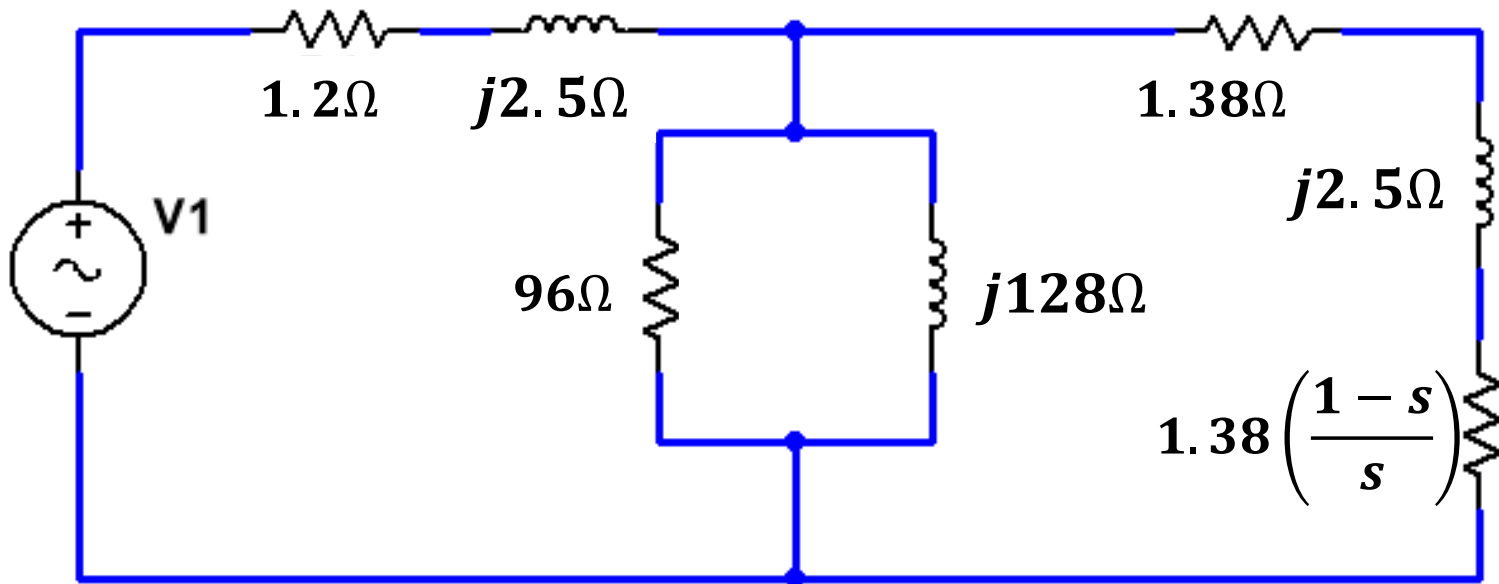
$$X_{eq} = \sqrt{(Z_{eq})^2 - (R_{eq})^2} = \sqrt{(5.63\Omega)^2 - (2.58\Omega)^2} = 5.0\Omega$$

$$X_{eq} = X_1 + X'_2 \qquad X_1 = X'_2 = \frac{X_{eq}}{2} = 2.5\Omega$$

Induction Motor Example

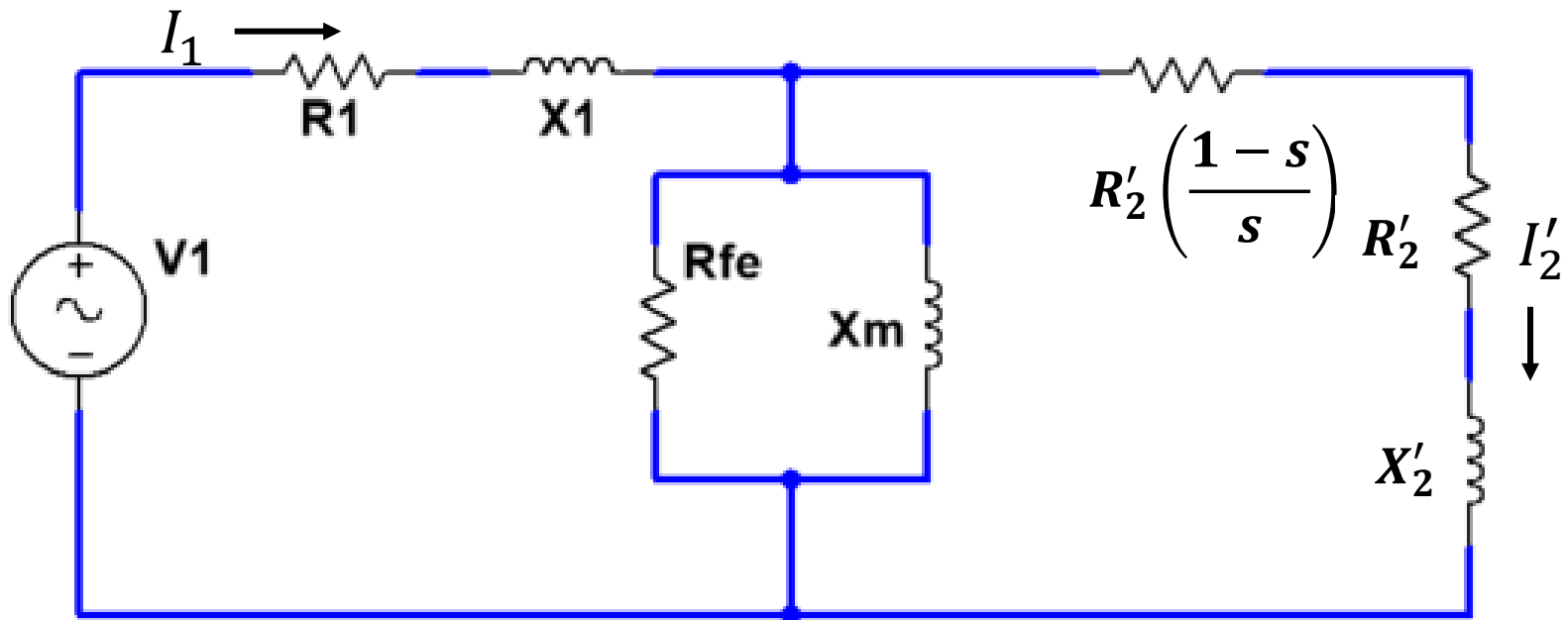
$$\tau = \frac{P_{mech}}{\omega_m}$$

$$P_{mech} = \tau \omega_m \propto 1.38 \left(\frac{1-s}{s} \right)$$



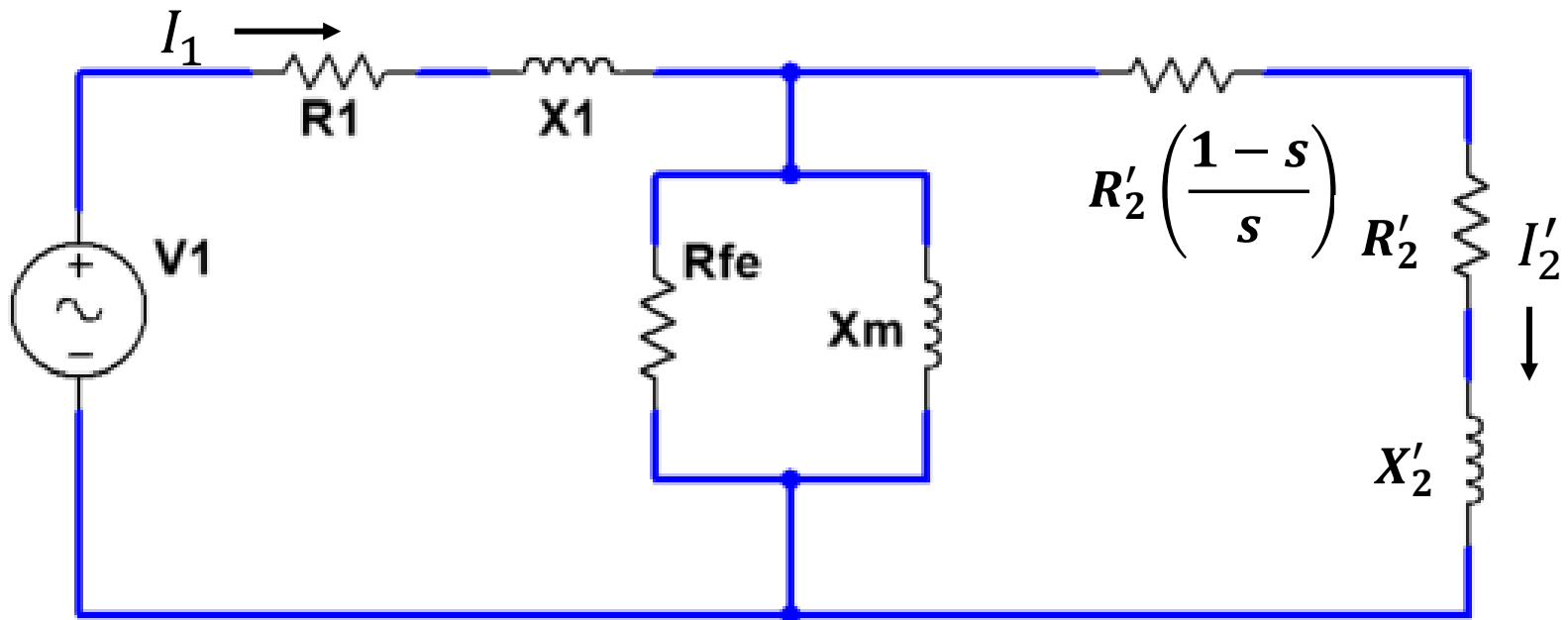
Induction Motor Efficiency & Slip

- Typically motor operates at highest efficiency at rated slip. This depends on armature winding and rotor construction.
- To get a better idea of how they are related, we return to our motor model.



Induction Motor Efficiency & Slip

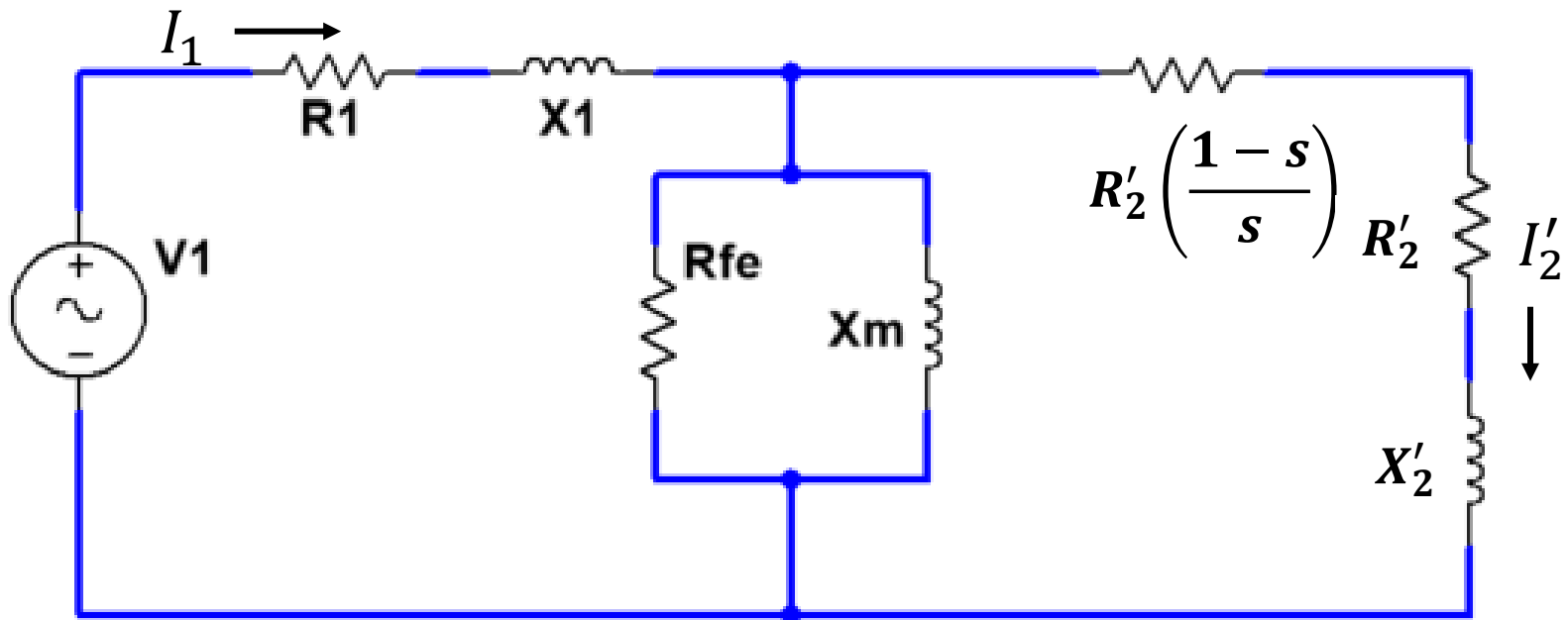
- We assume $R'_2 \ll R_{fe}$ and $X'_2 \ll X_m$, so we can neglect the core impedance and $I_1 \approx I'_2$
- We can then define $R_{eq} = R_1 + R'_2$ $X_{eq} = X_1 + X'_2$



Induction Motor Efficiency & Slip

- The mechanical power developed for all 3 phases is

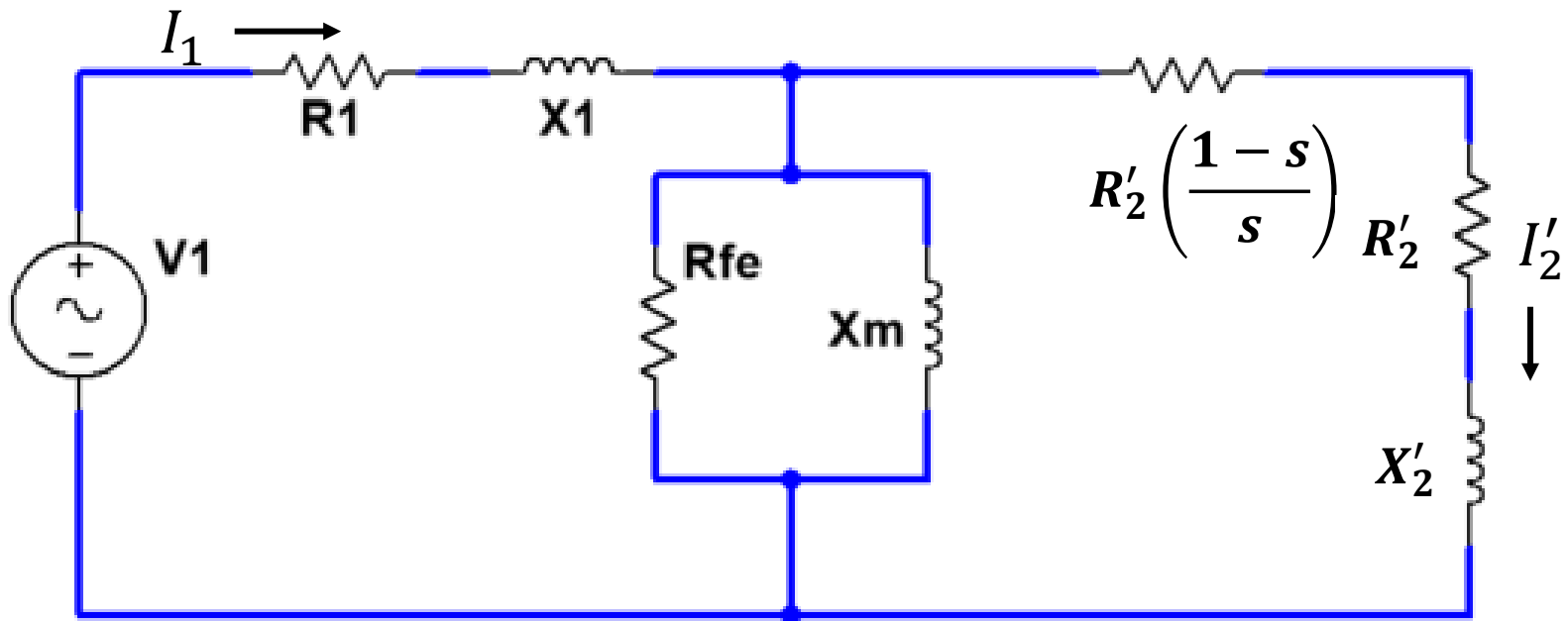
$$P_{mech} = 3(I'_2)^2 R'_2 \left(\frac{1-s}{s} \right)$$



Induction Motor Efficiency & Slip

- The current in terms of voltage is

$$I'_2 = \frac{V_1}{|R_{eq} + jX_{eq} + R'_2\left(\frac{1-s}{s}\right)|} = \frac{V_1}{\sqrt{R_{eq}^2 + X_{eq}^2 + \left[R'_2\left(\frac{1-s}{s}\right)\right]^2 + 2R_{eq}R'_2\left(\frac{1-s}{s}\right)}}$$



Induction Motor Power & Slip

- We can now write the developed mechanical power as

$$P_{mech} = \frac{3(V_1)^2 R'_2 \left(\frac{1-s}{s}\right)}{R_{eq}^2 + X_{eq}^2 + \left[R'_2 \left(\frac{1-s}{s}\right)\right]^2 + 2R_{eq} R'_2 \left(\frac{1-s}{s}\right)}$$

- If we want to find the slip at which we have maximum power, we can take the derivative and set it to zero. This yields:

$$R_{eq}^2 + X_{eq}^2 = \left[R'_2 \left(\frac{1-s}{s}\right)\right]^2$$

Induction Motor Power & Slip

- In terms of impedance,

$$Z_{eq} = R_{eq} + jX_{eq}$$

- Then

$$Z_{eq}^2 = R_{eq}^2 + X_{eq}^2 = \left[R'_2 \left(\frac{1-s}{s} \right) \right]^2$$

$$Z_{eq} = R'_2 \left(\frac{1-s}{s} \right)$$

- Putting this in terms of slip: $s_{Pmax} = \frac{R'_2}{R'_2 + Z_{eq}}$

Induction Motor Power & Slip

- Returning to our power equation,

$$P_{mech} = \frac{3(V_1)^2 R'_2 \left(\frac{1-s}{s}\right)}{R_{eq}^2 + X_{eq}^2 + \left[R'_2 \left(\frac{1-s}{s}\right)\right]^2 + 2R_{eq} R'_2 \left(\frac{1-s}{s}\right)}$$

- Then substituting in

$$s_{Pmax} = \frac{R'_2}{R'_2 + Z_{eq}}$$

- Yields and expression for maximum power:

$$P_{max} = \frac{3}{2} \left(\frac{(V_1)^2}{R_{eq} + Z_{eq}} \right)$$

Induction Motor Torque & Slip

- Recall our equation for torque $\tau = \frac{P_{mech}}{\omega_m} = \frac{P_{mech}}{s\omega_s}$

$$\tau = \frac{3(V_1)^2 \frac{R'_2}{s}}{\omega_s \left[R_{eq}^2 + X_{eq}^2 + \left[R'_2 \left(\frac{1-s}{s} \right) \right]^2 + 2R_{eq}R'_2 \left(\frac{1-s}{s} \right) \right]}$$

- If we want to find the slip at which we have maximum torque (that is the break-down torque), we can take the derivative and set it to zero. This yields:

$$s_{\tau max} = s_B = \frac{R'_2}{\sqrt{R_1^2 + X_{eq}^2}}$$

Induction Motor Torque & Slip

- We can then write the breakdown torque as

$$\tau_B = \tau_{max} = \frac{3(V_1)^2}{2\omega_s} \left[\frac{1}{R_1 + \sqrt{R_1^2 + X_{eq}^2}} \right]$$

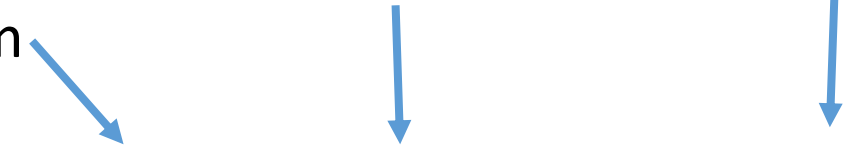
- Remember to keep units straight! Torque is in Newton-meters and power is in Watts.

Induction Motor Efficiency & Slip

- Since the developed mechanical power varies with slip, we would expect the efficiency, η , to vary as well.

$$\eta = \frac{P_{mech}}{P_{in}}$$

Mechanical power term Wire losses Core losses


$$P_{in} = \frac{3(V_1)^2 \left[R'_2 \left(\frac{1-s}{s} \right) + R_{eq} \right]}{R_{eq}^2 + X_{eq}^2 + \left[R'_2 \left(\frac{1-s}{s} \right) \right]^2 + 2R_{eq}R'_2 \left(\frac{1-s}{s} \right)} + \frac{3(V_1)^2}{R_{fe}}$$

Induction Motor Example

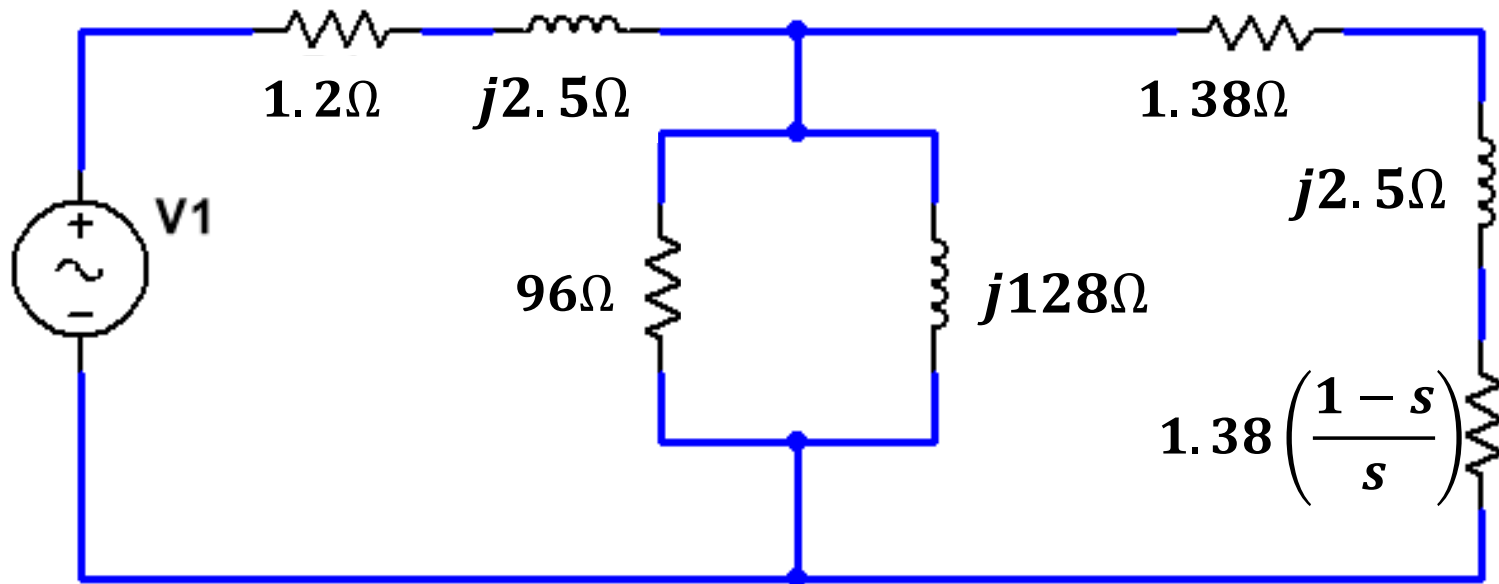
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Induction Motor Example

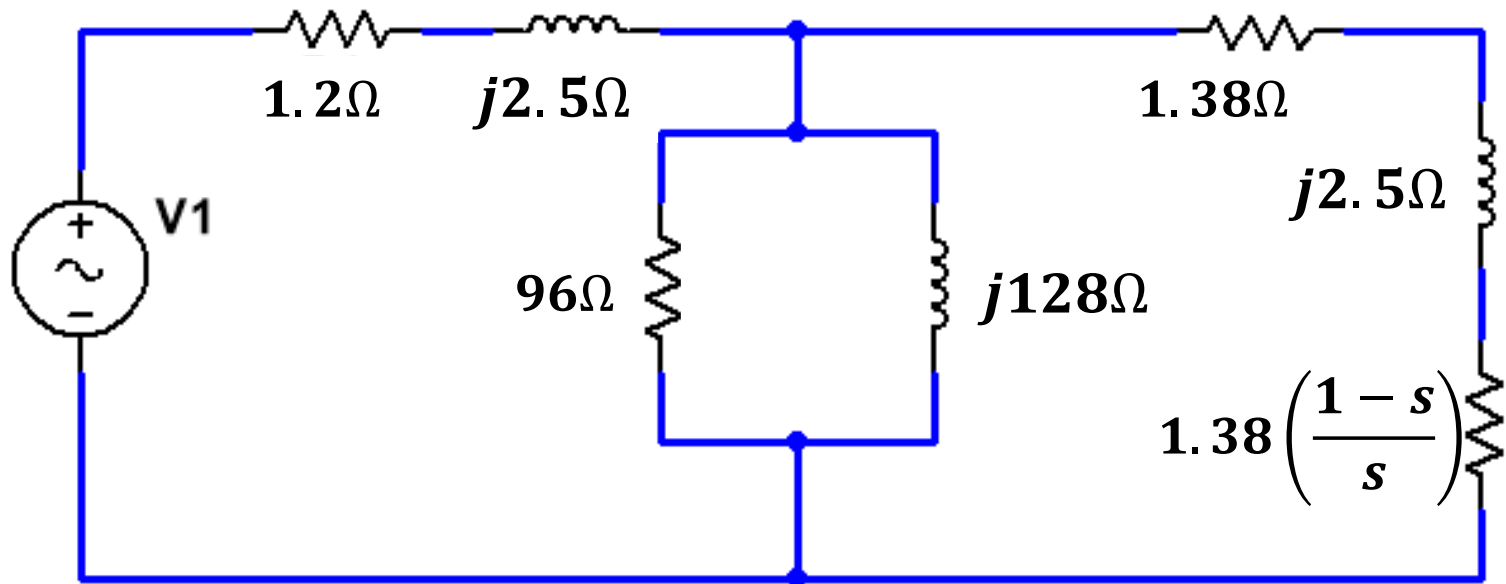
Rated slip is given by: $s = \frac{n_s - n_m}{n_s} = \frac{1800 - 1710}{1800} = 0.05$



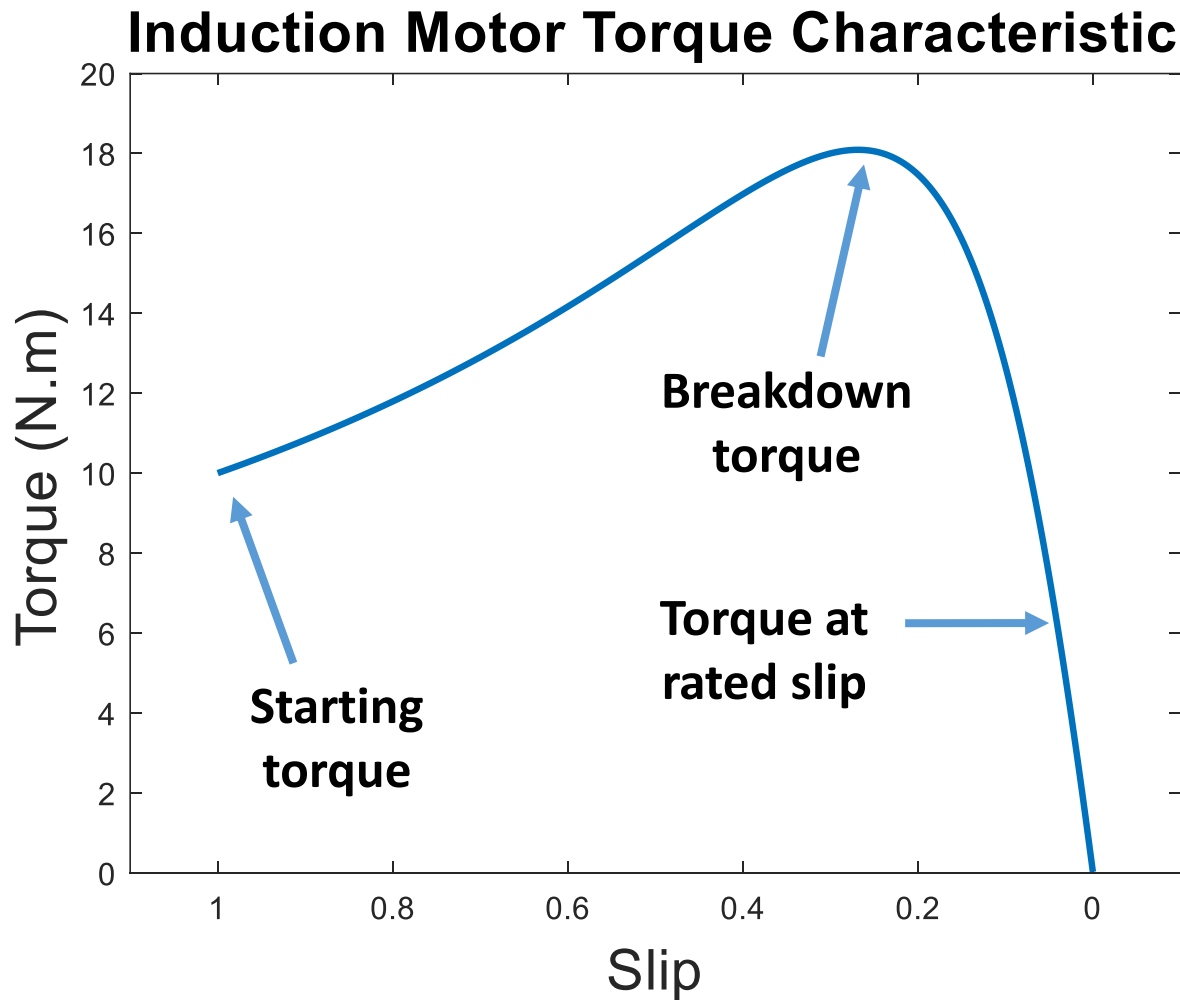
Induction Motor Example

Synchronous frequency for a 4-pole machine:

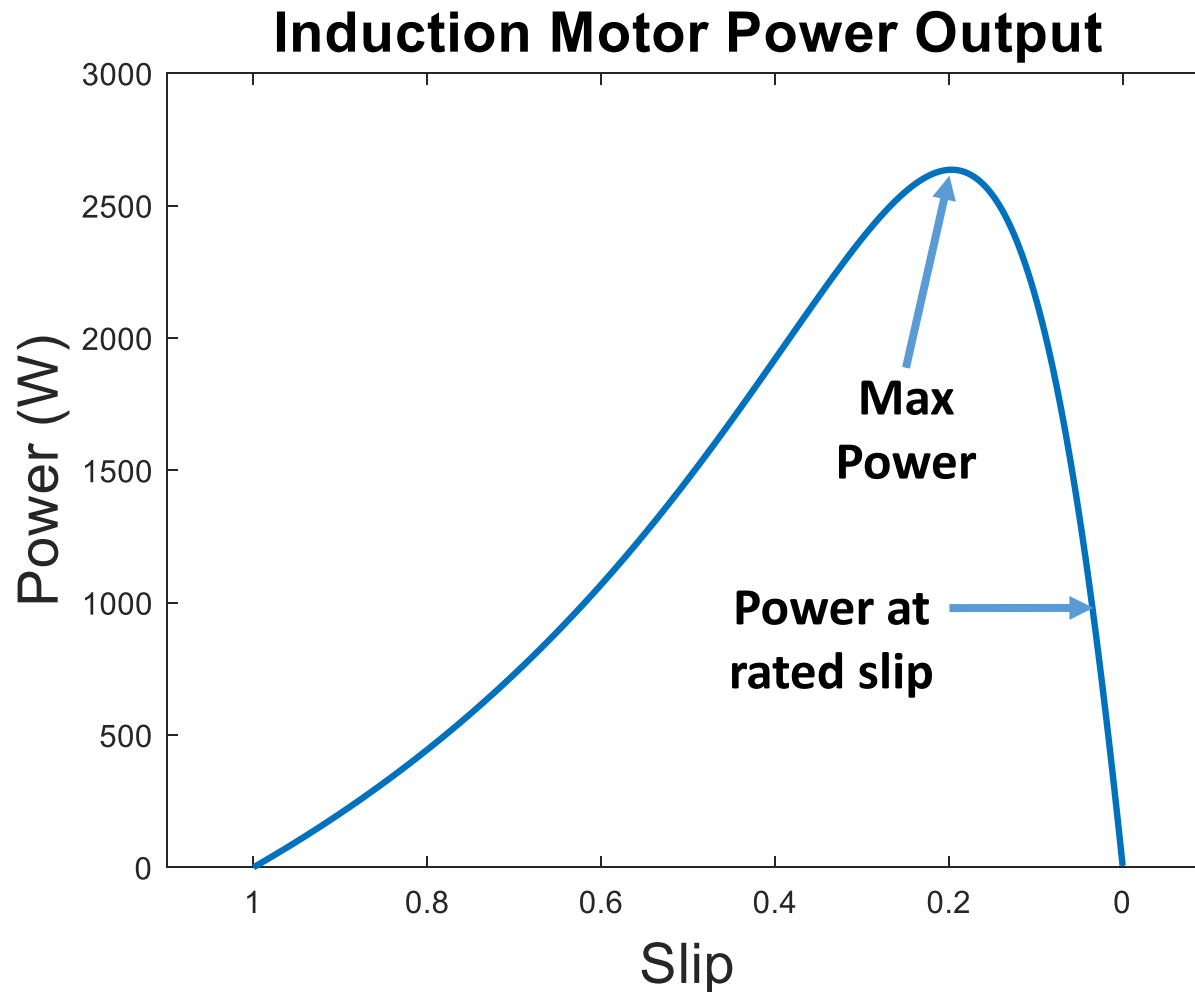
$$n_s = \frac{120f}{P} = \frac{120(60\text{Hz})}{4} = 1800\text{rpm}$$
$$\omega_s = \frac{n_s}{9.55} = 188.5 \text{ rad/s}$$



Induction Motor Example

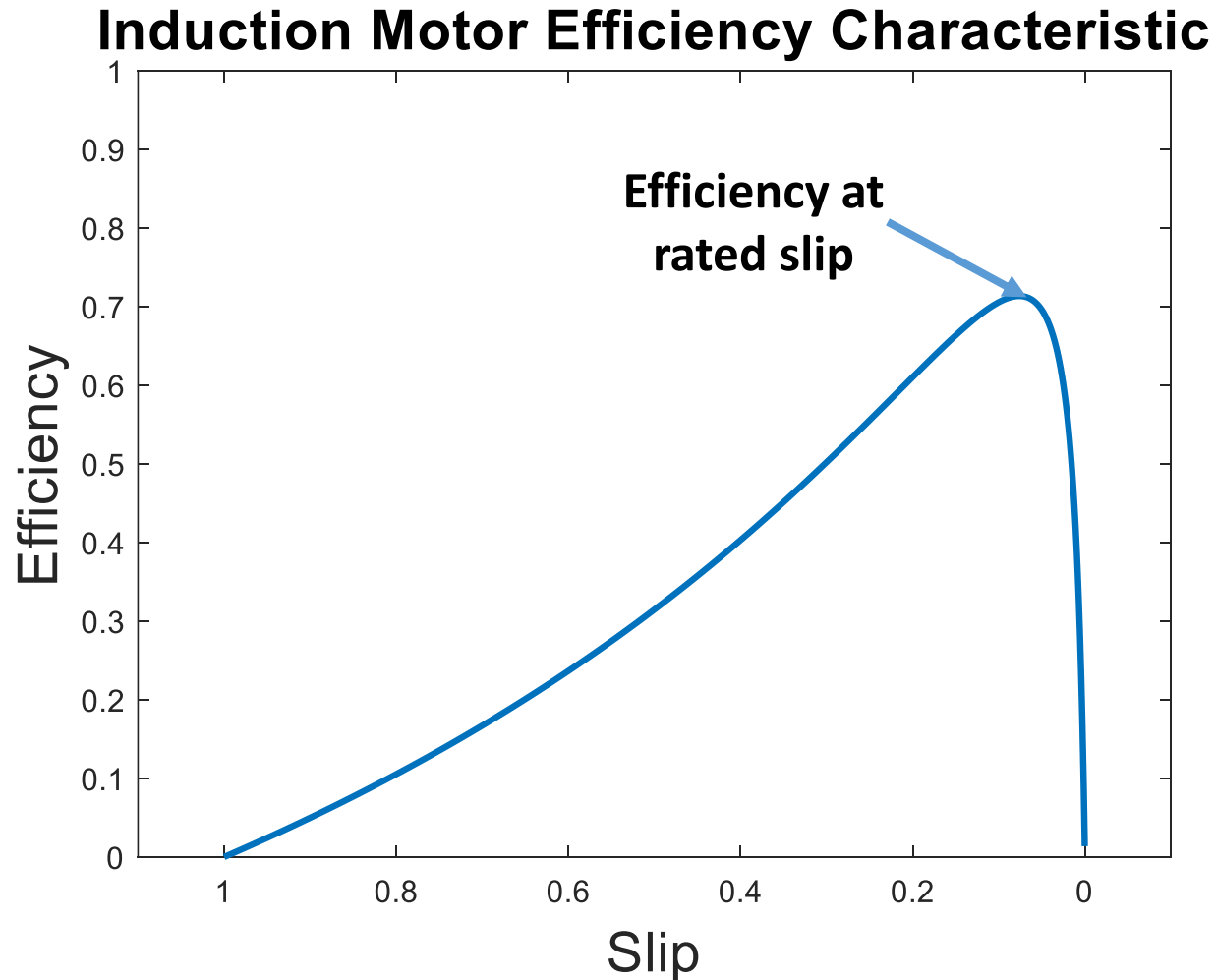


Induction Motor Example



Why is the rated slip not set for maximum power?

Induction Motor Example



Rated slip corresponds to optimal efficiency